Modeling of a Microstrip Low- Pass Filter by the Scattering-Bond Graph Formalism

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Abstract

Low pass filters play an important role in wireless systems. At the reception and the transmission, the signal has to be filtered at a certain frequency with a specific band width. In this paper we present a design of microstrip low- pass filter. The bond graph and the scattering formalism are used jointly to give an explicit model of filer.

The representations of transmission and reflection coefficients of filter are derived from the obtained model.

Keywords: Low Pass Microstrip Filter, Bond Graph Model, Scattering Formalism, Transmission and Reflection Characteristics.

1. Introduction

Electronics filters are required in all radio- frequency communication techniques. They are used to execute signal processing functions specifically to enhance the wanted frequency component, to remove the unwanted one [1]. There are four filter types: Low Pass Filters, High Pass Filters, Band Pass Filters and Band Stop Filters [2,3]. Depending on the characteristics and the conditions of application, the electronic filter can be designed by distributed or lumped elements [4].

In order to describe the physical behavior of a low pass microstrip filter, we will use a procedure which links the bond graph formalism to the scattering formalism. Firstly, we will develop a bond graph model of microstrip filter. Secondly, we will derive the scattering matrix from the reduced bond graph model. Finally, we will use the scattering parameters to extract the transmission and reflection characteristics by maple program.

2. Bond Graph Model

The Bond graphs are a kind of graphical language and systematic representation.

They were applied in physical multidiscipline domains, such as mechanics, electronics and hydraulics... They include elements and constitutive relations which can used to express the common energy transfer or transform behavior underlying the several physical domains.

The characteristics of bond graphs include:

• being able to obtain important qualitative information as a conceptual model.

• being able to reveal the relationships among system, subsystems, and elements.

• not only being able to represent the topology of subsystems or elements of different physical domains, but also being able to represent the relationships of their products among them.

The concepts of bond graphs include port and bond, elements, variables, constitutive relations and causality.

Fig.1 shows the concept of the basic bond graph component.

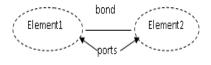


Fig. 1 Bond and ports of bond graph.

Between two elements, there is always a bond. Every bond has two power variables, one is effort (e), and the other is flow (f) associated with it. Energy will flow through the bond in either direction.



Bond graphs consist of nine types of elements, they are source of effort(Se), source of flow(Sf), inductor(I), capacitor(C), resistor(R), transformer(TF), gyrator(GY), 0-junction and 1-junction.

3. Proposed Structure and Bond Graph Model

The chosen structure, given by Fig 2, is a low pass microstrip filter formed by an alternating of high and low impedance transmission lines which are linked in cascade.

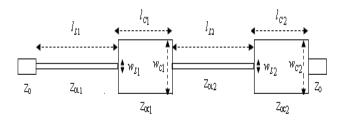


Fig. 2 Low pass microstrip filter

The physical characteristics of the filter are: $l_{L1} = l_{L2} = 9.8 \text{ lmm}, \ l_{C1} = l_{C2} = 7.1 \text{ lmm}$ $w_{C1} = w_{C2} = 4mm, \ w_{L1} = w_{L2} = 0.2mm$

The specifications of the filter are: $C_{1,2} = C_{1,2} = C_{1,2}$

Cut off frequency: fc=1.3GHz

Pass band ripple=0.1 dB

Source/load impedance: $Z0=50\Omega$

The characteristic impedances of high and low impedance lines are chosen as $ZOLi=93\Omega$ and $ZOCi=24\Omega$.

The substrate is characterized by a relative dielectric constant $\varepsilon_r = 10.8$ and a thickness $h = 1.27 \, mm$.

The narrow line with high impedance is equivalent to a lumped- element inductor attached in series.



Fig. 3 Microstrip line and its electric model.

$$L = \frac{Z_{0L} l_{Li}}{\upsilon_{pl}} \tag{1}$$

The large line with low impedance present a better approximation of lumped- element capacitor connected in parallel.

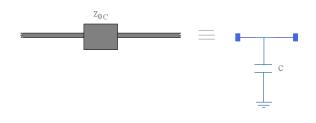


Fig. 4 Large microstrip line and its electric model.

 $C = \frac{l_{Ci}}{Z_{0C} \upsilon_{p2}}$

(2) Where

$$\mathcal{D}_{pi} = \frac{\omega}{\beta i} \tag{3}$$

And

$$\beta i = \frac{2\pi}{\lambda_{ai}} \tag{4}$$

 λ_{gi} The guided wavelength

Thus the equivalent circuit constituted by lumped elements is given by Fig. 5.

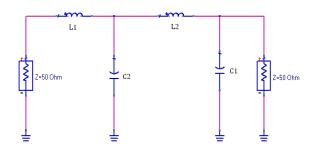


Fig. 5 Lumped elements filter

Applying the above formulas in our structure, we obtain:



The values of inductances: L1 = L2 = 7.7316 nHThe values of capacitances: C1 = C2 = 2.816 pF

So we can easily deduce the bond graph model of the filter. This model describes clearly the exchange of physical energy between the filter elements.

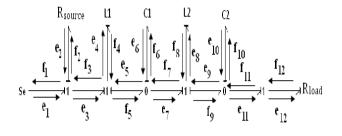


Fig. 6 Bond graph model.

From the bond graph model we can determine the Scattering parameters of filter. This approach is described in the next paragraph.

4. Derivation of the Scattering Matrix from Bond Graph Model

Scattering parameters or S-parameters describe the electrical behavior of linear electrical networks.

The researches of **Abdelkader Mami** and **Hichem Tghouti** [5, 6, 7, 8] have shown that it is possible to determine the scattering matrix of a system from its bond graph model.

In the case of the chosen structure, it is necessary to transform the bond graph model by a reduced bond graph model given by Fig. 7.

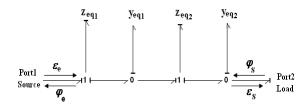


Fig.7 Reduced bond graph model.

Notice that:

 Z_{eqi} : The reduced equivalent impedance y_{eqi} : The reduced equivalent admittance

So we have:

$$z_{eq1} = r_1 + \tau_{L1}.s \tag{5}$$

$$y_{eq1} = \tau_{C1}.s \tag{6}$$

$$z_{eq2} = \tau_{L2}.s \tag{7}$$

$$y_{eq2} = \tau_{C2} \cdot s + r_2 \tag{8}$$

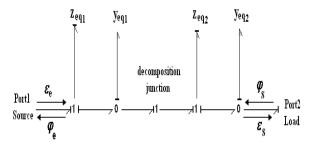
s: The Laplace operator.

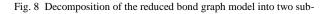
$$r_1 = \frac{R_{souce}}{R_0}$$
$$r_2 = \frac{R_{load}}{R_0}$$

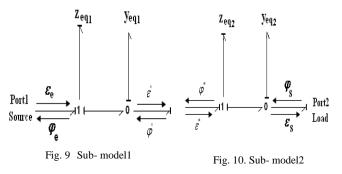
$$\tau_{Ci} = Ci.R_0 \tag{9}$$

$$\tau_{Li} = \frac{Li}{R_0} \tag{10}$$
$$R_0 = 50\Omega$$

The reduced bond graph model is easier to study by dividing it into two sub models.







$$B1 = -\frac{1}{z_{eq1}.y_{eq1}}$$
 (11): Loop gain of the algebraic

loop given by the first sub-model .

 $B2 = -\frac{1}{z_{eq2}.y_{eq2}}$ (12): Loop gain of the algebraic loop

given by the second sub-model

$$\Delta 1 = 1 + \frac{1}{z_{eq1} \cdot y_{eq1}}$$
(13): Determinant of causal

bond graph of the first sub-model.

$$\Delta 2 = 1 + \frac{1}{z_{eq2} \cdot y_{eq2}}$$
 (14): Determinant of causal

bond graph of the second sub-model.

The all integro- differentials [9,10] operators of the first sub model are:

$$\begin{cases} H_{11}[1] = \frac{y_{eq1}}{z_{eq1} \cdot y_{eq1} + 1} \\ H_{12}[1] = \frac{1}{z_{eq1} \cdot y_{eq1} + 1} \\ H_{21}[1] = \frac{1}{z_{eq1} \cdot y_{eq1} + 1} \\ H_{22}[1] = -\frac{z_{eq1}}{z_{eq1} \cdot y_{eq1} + 1} \\ \Delta(s)[1] = -\frac{1}{z_{eq1} \cdot y_{eq1} + 1} \end{cases}$$
(15)

The all integro- differentials operators of the second sub model are:

$$\begin{cases} H_{11}[2] = \frac{y_{eq2}}{z_{eq2} \cdot y_{eq2} + 1} \\ H_{12}[2] = \frac{1}{z_{eq2} \cdot y_{eq2} + 1} \\ H_{21}[2] = \frac{1}{z_{eq2} \cdot y_{eq2} + 1} \\ H_{22}[2] = -\frac{z_{eq2}}{z_{eq2} \cdot y_{eq2} + 1} \\ \Delta(s)[2] = -\frac{1}{z_{eq2} \cdot y_{eq2} + 1} \end{cases}$$
(16)

From these operators, we can deduce directly the wave matrix of the first and the second sub-model [11, 12,13].

$$W[1] = \begin{bmatrix} W_{11}[1] & W_{12}[1] \\ W_{21}[1] & W_{22}[1] \end{bmatrix}$$
(17)

$$W[2] = \begin{bmatrix} W_{11}[2] & W_{12}[2] \\ W_{21}[2] & W_{22}[2] \end{bmatrix}$$
(18)

Such as:

$$W_{11}[i] = \frac{1 - H_{11}[i] + H_{22}[i] - \Delta H[i]}{2H_{21}[i]}$$
(19)

$$W_{12}[i] = \frac{1 - H_{11}[i] - H_{22}[i] + \Delta H[i]}{2H_{21}[i]}$$
(20)

$$W_{21}[i] = \frac{1 + H_{11}[i] + H_{22}[i] + \Delta H[i]}{2H_{21}[i]}$$
(21)

$$W_{22}[i] = \frac{1 + H_{11}[i] - H_{22}[i] - \Delta H[i]}{2H_{21}[i]}$$
(22)

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$$\Delta H[i] = H_{11}[i]H_{22}[i] - H_{12}[i]H_{21}[i]$$
(23)

The global Wave matrix W_g is given by the product of W[1] and W[2] [14,15,16]:

$$W_{g} = W[1] * W[2] = \begin{bmatrix} W_{g}[11] & W_{g}[12] \\ W_{g}[21] & W_{g}[22] \end{bmatrix}$$
(24)

Then we can determine the S matrix[17]:

$$S = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$
⁽²⁵⁾

$$S_{11} = -\frac{W_g [12]}{W_g [22]} \tag{26}$$

$$S_{12} = \frac{1}{W_{g}[22]}$$
(27)

$$S_{21} = \frac{W_{g}[22]W_{g}[11] - W_{g}[12]W_{g}[21]}{W_{g}[22]}$$
(28)

$$S_{22} = \frac{W_s[21]}{W_s[22]}$$
(29)

A simple programming and simulation of the above scattering parameters equations, gives the Figures11- 14 which represent respectively the reflection and transmission coefficients of the studied filter.

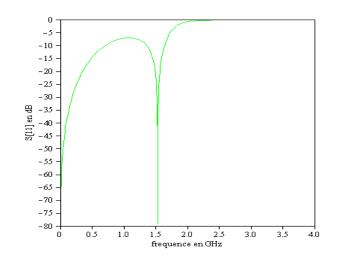


Fig. 11 Reflection coefficient S11

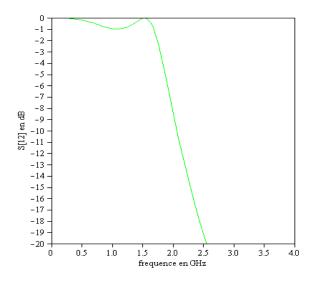


Fig. 12 Transmission coefficient S12



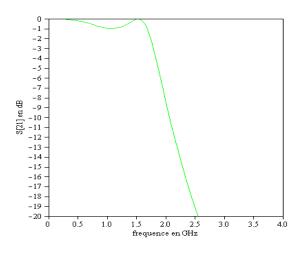


Fig. 13 Transmission coefficient S21

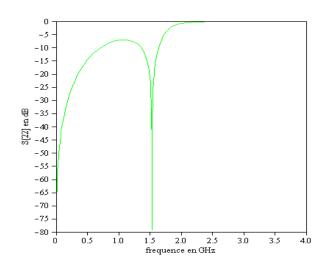


Fig. 14 . Reflection coefficient S22

The obtained results are in accordance with the characteristics of the filter, which proves the validity of the scattering bond graph formalism to analyze the linear systems.

5. Conclusions

In this article, we have used a procedure which links the bond graph formalism to the scattering formalism to analyze a low pass microstrip filter. Firstly, we have explained the method to find the bond graph model from the filter. Then, we showed the steps to obtain the S matrix. Afterwards, we have developed a maple program from the scattering parameters which has allowed us to represent the transmission and reflection characteristics.

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